

# LOCKE INSULATORS

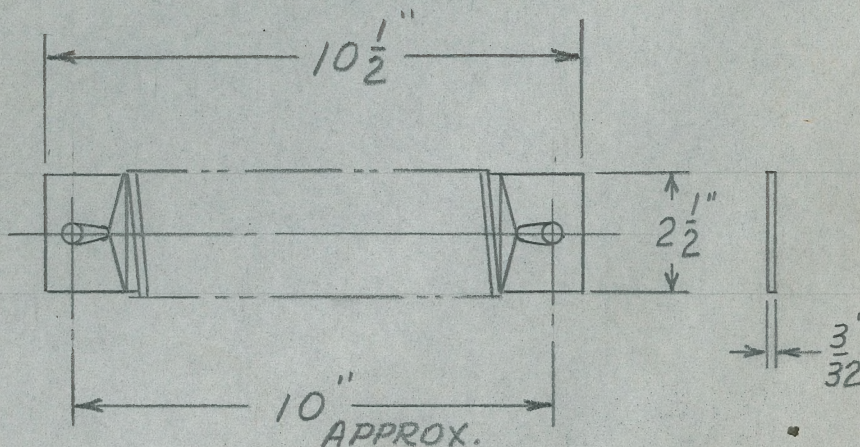
## REVISIONS

U-SK12-5-75-FCV

0 R 305 11-21-75  
DEC. 5, 1975

## TITLE

CARD RESISTOR - NON-INDUCTIVE



Mounting Hole  $\frac{1}{4}$ " dia.

PRINTS TO

MADE BY *EHW*  
APPROVALS

LOCKE INSULATORS, INC.  
BALTIMORE, MARYLAND 21230

U-SK12-5-75-FCV



REVISIONS

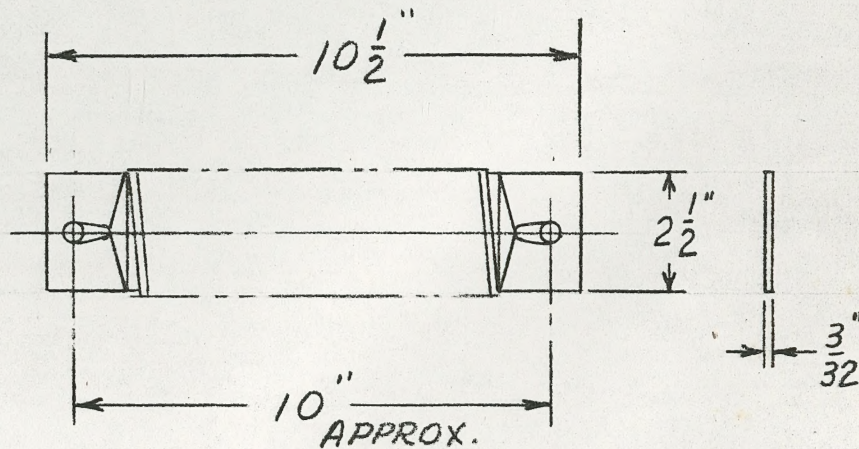
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INSULATORS  
**LOCKE**

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APPROVALS

LOCKE INSULATORS, INC.  
BALTIMORE, MARYLAND 21230

U-SK12-5-75-FCV



September 27, 1976

Mr. William Fields  
Building 42-2C  
General Electric Company  
100 Woodlawn Avenue  
Pittsfield, Massachusetts 01201

Dear Bill:

In accordance with our telephone conversation this past week, I would appreciate your giving us a quotation on making up noninductive resistor cards for use with our impulse generator, as follows:

<u>Number</u>	<u>Resistance (ohms)</u>
25	30
25	60
25	125
25	200
25	250
10	375

We have found that wire wound on a fiberglass material is quite satisfactory and does resist breakage to a considerable degree.

I am enclosing a sketch #U-SK12-5-75 FCV, which shows the dimensions of the cards we need.

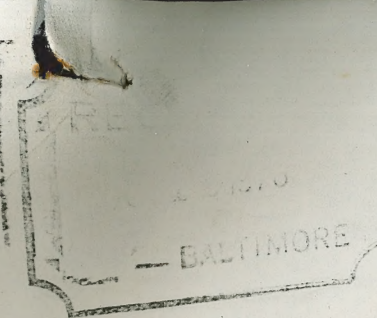
Please call me if you have any questions on Dial Comm: 8\*272-9235. Thank you for your cooperation.

Very truly yours,

F. C. Vose  
Manager-High Voltage  
Laboratory

FCV/lan  
enclosure





## SWITCHING SURGE CIRCUIT FOR LOCKE

The circuit for switching impulse testing is a modified lightning impulse testing circuit, as shown in Fig. 2. Salient modifications are:

- The tail resistance  $R_g$  and the resistance divider  $R_d$  are removed from the circuit. The long switching impulse tail is then formed by allowing the generator to discharge through the charging resistors  $R_c$ .
- The series resistance  $R_s$  is increased to produce the desired time to crest.
- The load capacitor  $C_L$  should be of the order of 1000 pF so that the series resistance does not become abnormally large.
- The load capacitor is used to form a capacitance voltage divider by connecting a low voltage, high capacitance capacitor between its lower end and ground.
- The load capacitor retains some charge following a switching impulse because the output gap of the generator stops conducting before the generator and  $C_L$  are completely discharged. This retained charge will cause the measurement of voltage on the next impulse to be somewhat incorrect. To circumvent this effect, bleeder resistors are connected in parallel with the load capacitors.

### Load Capacitors ( $C_L$ )

It is recommended that this be made up of (5) 138 kV coupling capacitors, Cat. No. 4CW35C5. Stacked in series, these will have a capacitance of about 1020 pF and an internal switching impulse strength of greater than 2400 kV. Each capacitor is 52-1/4 inches tall; therefore the height of the stack will be 261 inches. The stack will be mounted on an insulator of about one foot high similar to the arrangement of the present RIV capacitor stack. The positive polarity critical flashover voltage will be 1600 to 1700 kV. This could be increased to



about 2000kV by mounting the stack on a pedestal 7 ft. high. However, the strike distance from the impulse generator to the wall is 19.2 ft. and to the roof girders, 19.4 ft. The positive polarity CFO for these distances is about 1400 to 1500 kV, so there would be no advantage to putting the  $C_L$  on a pedestal.

On negative polarity it will be possible to work up to 2400 kV.

#### Series Resistance ( $R_S$ )

The standard switching impulse has a front of  $250 \pm 50 \mu s$  and a tail of  $2500 \pm 1500 \mu s$ .

With the proposed  $C_L$  of 1020 pF, a series resistance of 50 kilo-ohms is required to produce the  $250 \mu s$  front. This will consist of (50) 1000 ohm IRC resistors, Type RW11(175W). These resistors will operate satisfactorily at 50 kV so that 50 will be adequate for 2500 kV. It is proposed that 40 be installed in the generator and 10 external to the generator.

The resistors have ferrules so that they can be snapped into fuse clips like the present charging resistors. They are slightly shorter (9.5") than the present lightning impulse cards. It is suggested that fuse clips like those used for the charging resistors be installed in such a way that the switching impulse resistors and lightning impulse resistors can both be in place during lightning impulse tests and the latter be removed for switching impulse tests.

The (10) external resistors will be slipped onto a nylon or polypropylene rope. The rope is stretched and clamps attached to the rope at both ends. This keeps the ferrules in contact. Connection leads are attached to the ferrules at either end of the (10) resistors. The external resistors will be suspended from the impulse generator as the lightning impulse resistor now is.

#### Charging Resistors ( $R_C$ )

The present charging resistors are 5 kilo-ohms. They will need to be increased to 15 kilo-ohms in order to obtain a tail of 2500 to 3000  $\mu s$ .



### Capacitance Voltage Divider ( $C_L$ and $C_2$ )

The  $C_2$  capacitor in Figure 1 is used to control the ratio of the capacitance divider. It is proposed to establish ratios of approximately 8000, 5000, 3000, 2000, 1200. These will be used in the following manner.

A precision DC voltage supply will be used to provide a bias to the vertical deflection plates of the oscilloscope. This can be used to make accurate visual measurements of the voltage without taking oscillograms. For example, if the expected input voltage to the deflection plates is +450 volts, the bias is set to -450 volts. The operator then observes where the crest of the impulse is with respect to the zero line of the oscilloscope. If it coincides with the zero line, the impulse deflection is 450 volts. If it is 0.1 division low, the voltage is  $450 - (0.1 \times 50)$  or 445 volts. Reading accuracies of approximately 1% can be achieved.

When oscillograms are required, a lower input voltage and a lower bias voltage are used. The input voltage in this case will usually be in the range of 200 to 300 volts and the bias voltage in the range of 100 to 200 volts. In this case the internal bias can also be used in place of the external DC supply. The divider ratios will be used as shown below.

Test kV	Visual Reading		Oscillograms	
	Ratio	Oscil. Input Voltage	Ratio	Oscil. Input Voltage
2400 to 1500	5000	480 to 300	8000	300 to 188
1500 to 900	3000	500 to 300	5000	300 to 180
900 to 600	2000	450 to 300	3000	300 to 200
600 to 400	1200	500 to 330	2000	300 to 200



## C<sub>2</sub> Capacitor

The ratio of a capacitance divider is

$$\text{Ratio} = \frac{C_1 + C_2}{C_1}$$

and where  $C_2 \gg C_1$

$$\text{Ratio} = \frac{C_2}{C_1}$$

The exact value of  $C_1$  will have to be determined after the capacitors have been acquired. It should be close to 1020 pF. Using this value, the  $C_2$  capacitances will be:

<u>Ratio</u>	<u>C<sub>2</sub> (uF)</u>
8000	8.16 (5 & 3 in parallel)
5000	5.1
3000	3.06
2000	2.04
1200	1.22

The  $C_2$  capacitors are mounted in a 3" x 4" x 5" minibox as shown in photographs 1 and 2 and Figure 2. The parts are as follows:

1. Capacitors
2. Bleeder Resistor
3. Banana Plug Receptacle - Insulated
4. Banana Plug Receptable - Grounded
5. Lead to Amphenol Connectors
6. Ground Collector Ring
7. Tabs of Collector Ring
8. Amphenol Female Connector
9. 1/4 x 20 Bolts and Nuts



The connection from  $C_1$  to  $C_2$  is made via the insulated banana plug receptacle, item 3. The connection to ground is made via the 1/4-20 bolt and nut, item 9. The capacitors, several in parallel, are arranged in a circular bundle, item 1. At one end, their leads are connected together and then connected to the insulated banana plug and also to the Amphenol connection via a wire that runs centrally through the cluster of capacitors. A 200 kilo-ohm, one-watt resistor is connected from the insulated banana plug connection to the grounded banana plug. In the photograph a toggle switch is shown in series with this resistor. The switch is used to disconnect the resistor when the divider is used to measure sixty-hertz voltages.

The ground collector ring can be made from a short length of 1-1/2" copper tubing, one end of which is sawed and formed into supporting feet which are bolted to the minibox with the 1/4 x 20 bolts.

The 8  $\mu F$   $C_2$  will be obtained by using the 5 and 3  $\mu F$  units in parallel. Both will be connected to the bottom end of the  $C_L$  and the deflection cable will be connected to the 5  $\mu F$  unit.

#### Bleeder Resistors ( $R_L$ ) For Load Capacitors

These resistors are shown in photograph 3. They are made up of a number of 680 kilo ohm, 2 watt carbon resistors. The resistors are mounted in a zigzag pattern on a strip of insulating material 2-1/2" wide and the height of one capacitor in length. Holes are drilled 1/4" in from the edge and spaced so as to give a pitch of 1-1/2" to the zigzag. Connection pins are placed in the holes and the resistors soldered into place.

Since the capacitors are 52-1/4 inches tall, the number of resistors per capacitor will be about  $50/0.75$  or 67. The end plates of the capacitors are drilled and tapped to support the strips and make electrical connections.

#### Precision DC Power Supply

This is a Fluke 412B power supply rated 2100 volts, 30 mill-amperes. This is more voltage than needed but they have discontinued the lower voltage units.



The power supply will be connected to the binding post at the top rear of the 507 oscilloscope and the Position Mode knob will be turned to External.

#### Oscilloscope

When testing, the attenuator switch on the 507 scope must be in the direct position in order to disconnect the 75 ohm terminating impedance. No ratio adjustments can be made at the oscilloscope. Sweep speeds for switching surge waves are usually selected as 50  $\mu\text{s}/\text{cm}$  or 100  $\mu\text{s}/\text{cm}$  for viewing the front and 200 or 500  $\mu\text{s}/\text{cm}$  for viewing the tail. For reading the crest of wave, 100  $\mu\text{s}/\text{cm}$  is a good compromise.

A. F. Rohlfs  
October 7, 1976

-ng

Attach.

cc: JG Anderson  
FJ Turner



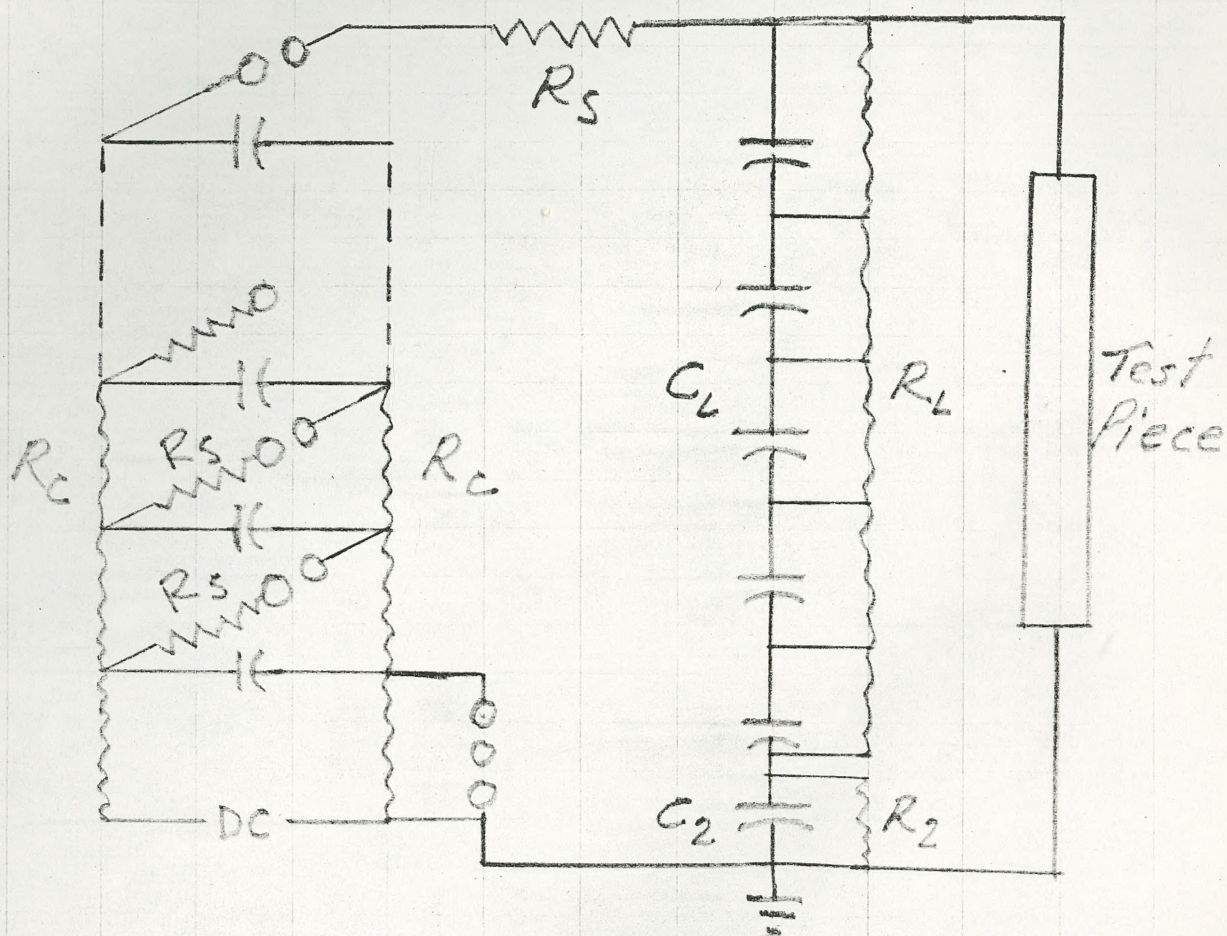


FIG 1 - SWITCHING IMPULSE  
CIRCUIT



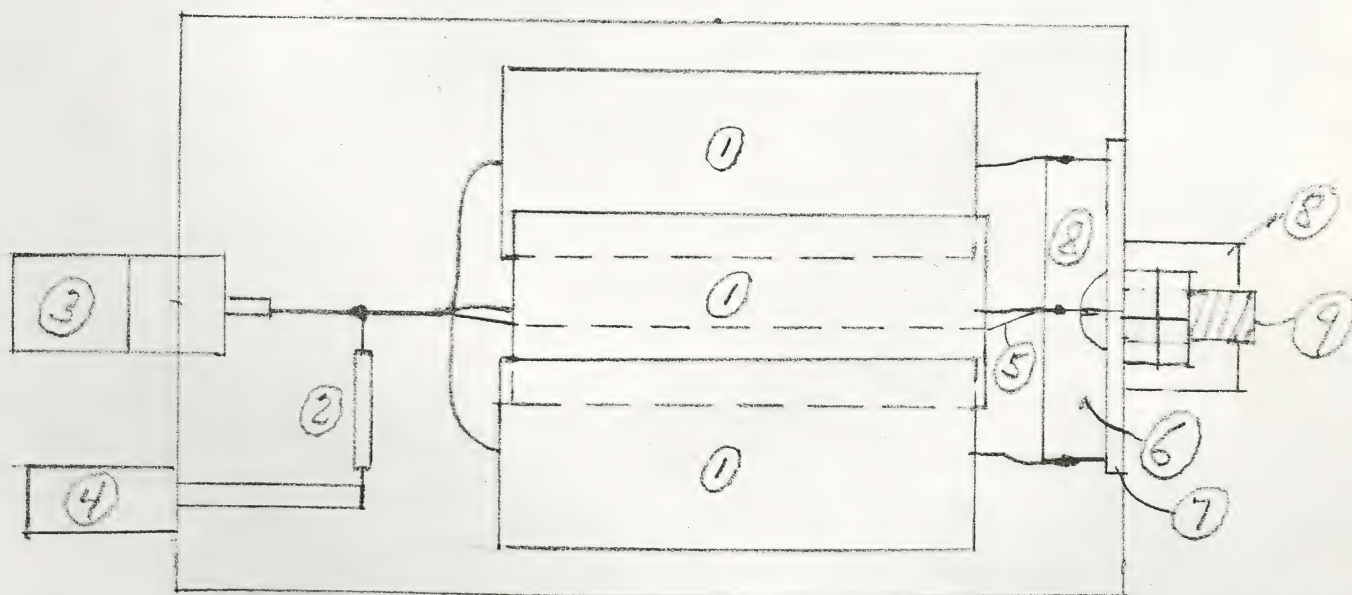
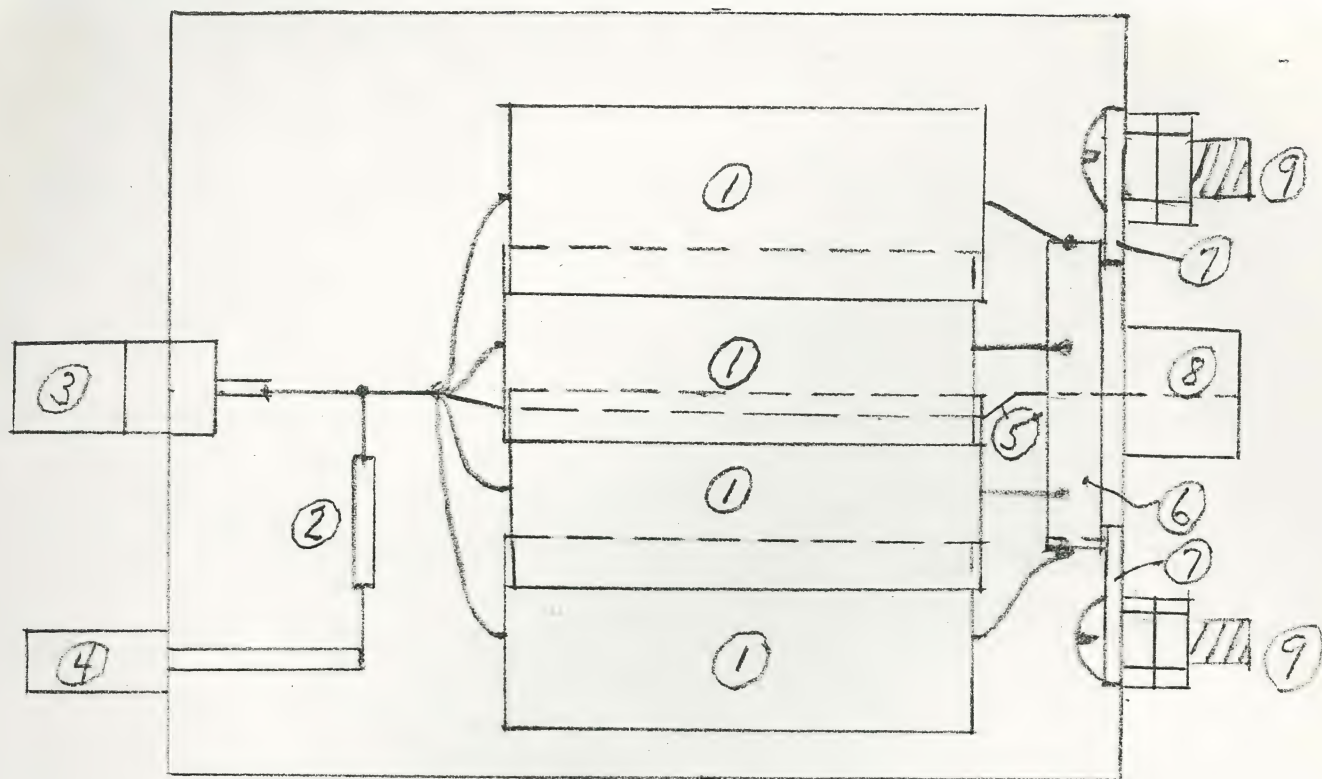
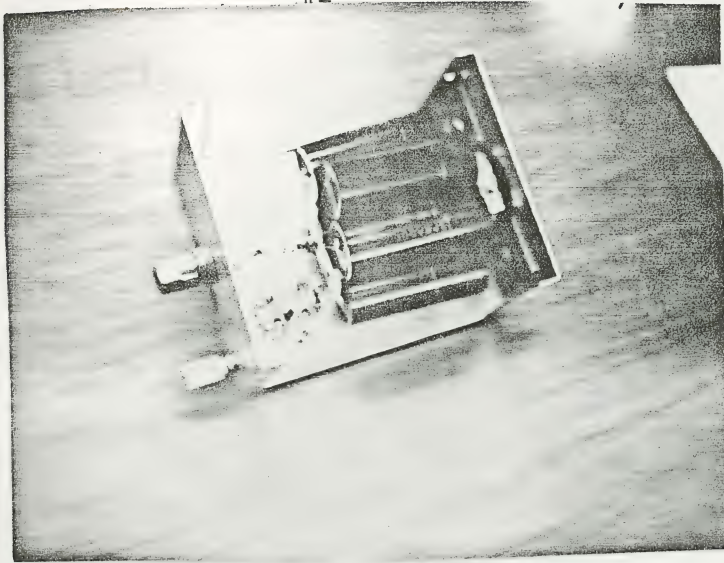


FIG. 2 - C<sub>2</sub> BOX

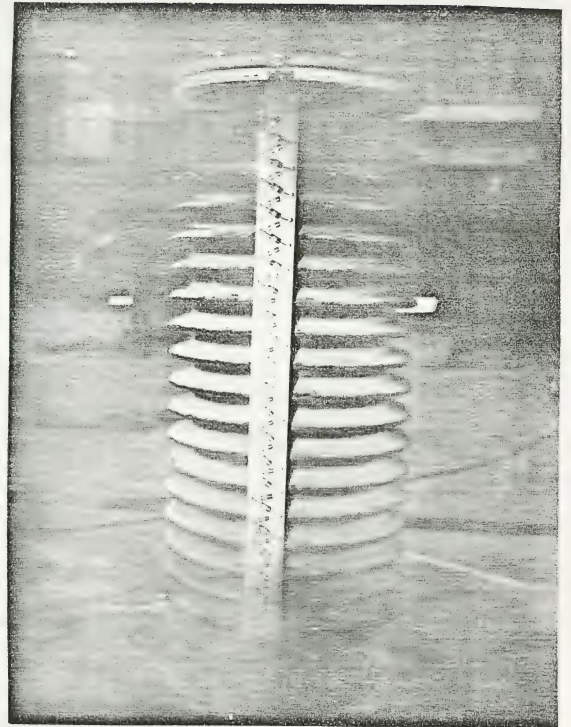
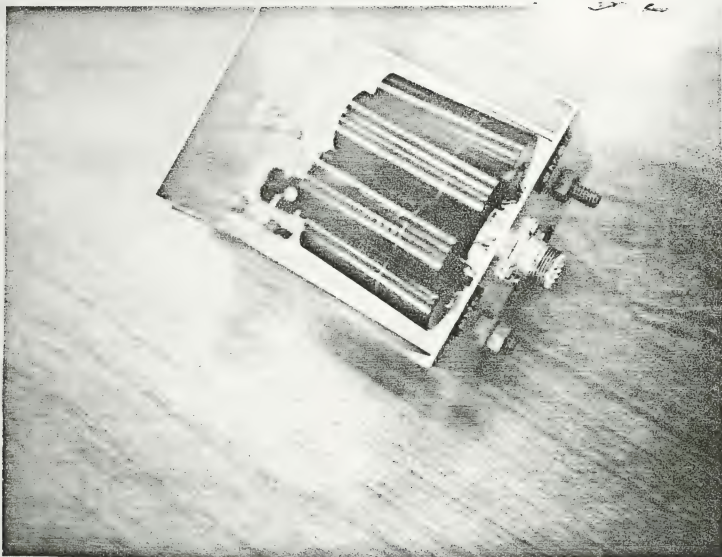
Full Scale  
AFRohifs  
9/9/76



#1



#2



#3



## COSTS

### Load Capacitor ( $C_L$ )

(5) GE Cat. No. 4CW35C5 coupling capacitors @ \$1381. \$ 6,905

Delivery 10-12 weeks

### Series Resistance ( $R_S$ )

(50 + 20 spare) 1000 ohm IRC resistors Type RW11 (175 watts) @ \$4.25. 298

Delivery 6-8 weeks.

Add mounting clips in generator In House

\$ 7,203

### Charging Resistors ( $R_C$ )

(124 + 26 spares) 15000 ohm IRC resistors, Type RW11 (175 watts) @ \$4.75 713

Delivery 6-8 weeks

713

### $C_2$ Capacitors

#### 5 $\mu$ F and 3 $\mu$ F units

(8 + 2 spares) 1  $\mu$ F, 600 volts Sprague Type 161P Black Beauty capacitors @ \$2.00 20

#### 2 $\mu$ F units

(4 + 1 spare) 0.5  $\mu$ F, 600 volts Sprague Type 161 P Black Beauty capacitors @ \$1.50 8



1.2 uF Unit

(6 + 1 spare) 0.2 $\mu$ F, 600 volts Sprague Type 161 P Black Beauty capacitors @ \$1.00	\$ 7
(4 + 2 spares) 200 kilo ohms (1 watt) Bleeder Resistors	
(4 + 1 spare) Insulated Banana Plug Plug Receptacle	
(4 + 1 spare) Grounded Banana Plug Receptacle	20
(4 + 1 spare) chassis mounted Amphenol	
(4) Female Connectors UHF 83-1R	
Miniboxes	
Miscellaneous Hardware	

---

55

Bleeder Resistors ( $R_L$ )

(335 + 65 spares) 680 kilo ohms, 2 watt carbon resistors (10% tolerance)	400
Insulating strips Connection pins Miscellaneous hardware	20

---

420

Precision DC Power Supply

(1) Fluke 412B DC power supply 2160 volts, 30 milliamperes	745
Delivery 2 weeks	



Where to order major items

Load Capacitor ( $C_L$ )

General Electric Co.  
Lynchburg, Va.

Can contact Bob Aideldinger - 8-272-2418

Series Resistors and Charging Resistors

IRC Boone Division  
Greenway Rd.  
P. O. Box 393  
Boone, N. C. 28607

Tel. (704) 264-8861

$C_2$  Capacitors

Sprague Electric Co.  
North Adams, Mass.

Precision DC Power Supply

John Fluke Mfg. Co., Inc.  
P. O. Box 43210  
Mount Lake Terrace  
Washington, D. C. 98043

Tel. (206) 774-2211

27  
A. F. Rohlfs  
October 7, 1976



SHIP TO  
(SEE SHIPPING INSTRUCTIONS BELOW)

# LOCKE

2525 INSULATOR DRIVE  
BALTIMORE, MARYLAND 21230

**Phone (301) 752-8020**

DATE	ROUTING	MARK ALL DOCUMENTS & PACKAGES FOR GATE NO.	PURCHASE ORDER NO. 82717
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DELIVERY REQUIRED	TERMS	F.O.B.	ADDRESS ALL CORRESPONDENCE TO 2525 INSULATOR DRIVE BALTIMORE, MD. 21230 Attn.
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ITEM	QUANTITY	DESCRIPTION	PRICE
		Performs Switching Transfer Flashes Tests at House Holding of Supervisors Translators in accordance with the Bonneville Power Administration Specifications, upon the Translator furnished by Lake Mead Tests scheduled to begin Oct 25, 1976	

☐ SUBJECT TO MARYLAND SALES OR USE TAX      ☐ NOT SUBJECT TO MARYLAND SALES OR USE TAX LICENSE NO. B-82993

APPROVED BY \_\_\_\_\_

AUTHORIZED SIGNATURE

**COMMENTS:**

2814 de

DATE ORDERED 10/1/76	DATE WANTED 10/25/76	DELIVER TO H. V. Lab	SIGNED (REQUESTORS) Vary	APPROVALS SE Gentry
SUGGESTED VENDORS				

## SUGGESTED VENDORS

1. High Voltage Laboratory
2. IPE Co. Pittsfield Mass
3. Arthur H. Ford Turner

EST. COST

ACCOUNT NO.

29102-5-28-98

VERBAL ☐ INVOICE APPROVAL

REQUESTOR'S COPY 1



# SWITCHING IMPULSE TESTS

Cat 365355 G 402

5-3.2 SWITCHING IMPULSE FLASHOVER CHARACTERISTICS OF INSULATOR STRINGS. The rated critical-impulse flashover voltage with a positive polarity 150/2500 switching impulse shall be as shown below for the insulator strings specified:

a. Twenty-unit string of 6-1/4 x 11-inch, 56,000 lb M and E rating insulators and

Nineteen-unit string of 6-1/2 x 12-5/8-inch, 40,000 lb M and E rating insulators:

1210 kV, dry; 1150 kV, wet

b. Twenty one-unit string of 7-3/4 x 12-5/8-inch, 56,000 lb M and E rating insulators:

1400 kV, dry; 1450 kV, wet

Plan 5 - Three strings of each size per 3-3.2 made up of randomly chosen units will constitute a sample. If any string fails to meet the requirement, a second sample of six more strings shall be tested. If any string of the second sample fails, the design shall be rejected.

Plan 6 - Sample size shall be five units.

5-5.1.11 Switching Impulse Tests. Insulators from the first lot shall be subjected to switching impulse tests. The tests shall be performed on the insulator strings specified in 3-3.2 in accordance with the procedures specified below to determine the critical-impulse flashover voltage.

5-5.1.11.1 Each string of insulators shall be subject to switching impulses under both dry and wet conditions with a positive polarity 150/2500 wave. Switching impulse tests shall be performed in accordance with the applicable procedures of ANSI C29.1, C68.1, and C68.2. Oscillographic records shall be furnished as part of the test report. Failure of the average critical-impulse flashover value of the strings to equal or exceed 92 percent of the rated critical-impulse flashover value specified in 3-3.2 shall constitute failure to meet the requirements of the switching impulse tests.

Ed Schramm  
Al Roberts  
Fred Turner

2775

PO-22717



LOCKE INSULATORS, INC.

AUTHORIZATION AND EXPENDITURE RECORD

CHG. ACCT. NO. 293-370-01  
 DATE ISSUED Sept. 3, 1976  
 DATE COMPLETED \_\_\_\_\_

AUTHORIZATION NO. 293-370-01  
 EST. COST: MATERIAL \_\_\_\_\_  
 LABOR \_\_\_\_\_  
 OUTSIDE EXPENDITURE \_\_\_\_\_  
 TOTAL \$2,500.00

REMARKS Development Authorization

PLEASE AUTHORIZE THE FOLLOWING: (SHOW IN BODY COMPLETE DETAIL OF EXPENDITURE AND WORK TO BE DONE)  
 PLEASE DO THE FOLLOWING WORK:

This authorization is written to cover the cost of Consultation Service of Mr. Al Rolphs, General Electric Co., Pittsfield, Massachusetts, and associated travel costs from Pittsfield to Baltimore and return.

The consultation and associated services are for the purpose of establishing the capability of making Switching Surge Tests in the High Voltage Laboratory in Baltimore.

*PO # 22347 covers service*

*1<sup>st</sup> Bill Invoice M-5808 11/24/76 445.73*

SEP 7 1976

DISTRIBUTION: BE Kingsbury  
 FC Vose  
 General Acctg.

Cost  
 Purchasing

ISSUED BY: Fred C. Vose  
 APPROVED BY: F. C. Vose  
[Signature]



# LOCKE INSULATORS, INC.

## AUTHORIZATION AND EXPENDITURE RECORD

CHG. ACCT. NO. See Below  
 DATE ISSUED Oct. 18, 1976  
 DATE COMPLETED December, 1976

AUTHORIZATION NO. 768  
 EST. COST: MATERIAL  
 LABOR  
 OUTSIDE EXPENDITURE \$3 750  
 XXXXXX 10% Contingency 375  
 TOTAL \$4 125

REMARKS XXXXXXXXXXXXXXXXXXXXXXXXXXXX  
Program #98 Category I

PLEASE AUTHORIZE THE FOLLOWING: (SHOW IN BODY COMPLETE DETAIL OF EXPENDITURE AND WORK TO BE DONE)  
 PLEASE DO THE FOLLOWING WORK:

Funds are requested to purchase the required material and have fabricated certain special components to give the High Voltage Laboratory the equipment to make Switching Surge tests.

### Cost Analysis

<u>Item</u>	<u>Investment</u>	<u>Expense</u>	<u>Total</u>
Series Resistors	--	325	325
Charging Resistors	--	725	725
Bleeder Resistors	--	400	400
Capacitors and Hardware	--	200	200
Miscellaneous Hardware	--	500	500
Labor for Making Capacitor			
Boxes & Resistor Banks	--	800	800
D.C. Power Supply	<u>800</u>	<u>--</u>	<u>--</u>
SubTotals	800	2 950	3 750
10% Contingency	<u>80</u>	<u>295</u>	<u>375</u>
Totals	<u>880</u>	<u>3 245</u>	<u>4 125</u>

### CHARGE ACCT. NO.

INVESTMENT - 768-293-890-1-98  
 490 TAX ON INVEST - 293-383-05-768-98  
 MODIFY EQUIP. - 293-356-01-768-98  
 NEW MISC. EQUIP. - 293-303-01-768-98

DISTRIBUTION: FC Vose  
 BE Kingsbury  
 General Accounting

Cost  
 Machine Shop

ISSUED BY: Fred C. Vose

APPROVED BY: B. S. Smith

10/19



# LOCKE INSULATORS, INC.

## AUTHORIZATION AND EXPENDITURE RECORD

CHG. ACCT. NO. SEE BELOW  
 DATE ISSUED Oct. 18, 1976  
 DATE COMPLETED December, 1976

AUTHORIZATION NO. 768  
 EST. COST: MATERIAL  
 LABOR  
 OUTSIDE EXPENDITURE  
 \$3 750  
 XXXXXX 10% Contingency 375  
 TOTAL \$4 125

REMARKS XXXXXXXXXXXXXXXXXXXX  
Program #98 Category I

PLEASE AUTHORIZE THE FOLLOWING: (SHOW IN BODY COMPLETE DETAIL OF EXPENDITURE AND WORK TO BE DONE)  
 PLEASE DO THE FOLLOWING WORK:

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<u>Item</u>	<u>Investment</u>	<u>Expense</u>	<u>Total</u>
Series Resistors	--	325	325
Charging Resistors	--	725	725
Bleeder Resistors	--	400	400
Capacitors and Hardware	--	200	200
Miscellaneous Hardware	--	500	500
Labor for Making Capacitor Boxes & Resistor Banks	--	800	800
D.C. Power Supply	<u>800</u>	--	--
SubTotals	800	2 950	3 750
10% Contingency	<u>80</u>	<u>295</u>	<u>375</u>
Totals	<u>880</u>	<u>3 245</u>	<u>4 125</u>

### CHARGE ACCT. NO.

INVESTMENT - 768-293-890-1-98  
 4% TAX ON INVEST - 293-383-05-768-98  
 MODIFY EQUIP. - 293-356-01-768-98  
 NEW MISC. EQUIP. - 293-303-01-768-98

DISTRIBUTION: FC Vose  
 BE Kingsbury  
 General Accounting

Cost  
 Machine Shop

ISSUED BY: John C. Vose

APPROVED BY: 10/19



# SWITCHING IMPULSE TESTS

36,000 lb insulator

*Brunner*  
*Sept*  
*Show it in*

3-3.2 SWITCHING IMPULSE FLASHOVER CHARACTERISTICS OF INSULATOR STRINGS. The rated critical-impulse flashover voltage with a positive polarity 150/2500 switching impulse shall be as shown below for the insulator strings specified:

a. Twenty-unit string of 6-1/4 x 11-inch, 36,000 lb M and E rating insulators and

Nineteen-unit string of 6-1/2 x 12-5/8-inch, 40,000 lb M and E rating insulators:

1210 kV, dry; 1130 kV, wet

b. Twenty one-unit string of 7-3/4 x 12-5/8-inch, 36,000 lb M and E rating insulators:

1630 kV, dry; 1450 kV, wet

Plan 5 - Three strings of each size per 3-3.2 made up of randomly chosen units will constitute a sample. If any string fails to meet the requirement, a second sample of six more strings shall be tested. If any string of the second sample fails, the design shall be rejected.

Plan 6 - Sample size shall be five units.

3-5.1.11 Switching Impulse Tests. Insulators from the first lot shall be subjected to switching impulse tests. The tests shall be performed on the insulator strings specified in 3-3.2 in accordance with the procedures specified below to determine the critical-impulse flashover voltage.

3-5.1.11.1 Each string of insulators shall be subject to switching impulses under both dry and wet conditions with a positive polarity 150/2500 wave. Switching impulse tests shall be performed in accordance with the applicable procedures of ANSI C29.1, C68.1, and C68.2. Oscillographic records shall be furnished as part of the test report. Failure of the average critical-impulse flashover value of the strings to equal or exceed 92 percent of the rated critical-impulse flashover value specified in 3-3.2 shall constitute failure to meet the requirements of the switching impulse tests.

2775





TRANSFORMER AND  
DISTRIBUTION  
EQUIPMENT  
BUSINESS DIVISION

GENERAL ELECTRIC COMPANY, 100 WOODLAWN AVE., PITTSFIELD, MASS. 01201  
Phone (413) 494-3577  
(EXT.)

August 12, 1976

Mr. F. C. Vose  
Locke Insulators, Inc.  
2525 Insulator Drive  
Baltimore, Md. 21230

Dear Fred:

John Anderson has asked me to reply to your request for someone from the High Voltage Laboratory to help you get set up for switching surge testing. That person will be either Fred Turner or me.

I estimate that it will cost \$2000 plus the cost of one or possibly two trips to Baltimore. The first trip would be to get familiar with your laboratory. The second trip might be needed to assist in the final set up. I would anticipate that one day would be spent in Baltimore on each trip. The rest of the time would be spent in Pittsfield preparing specifications and sketches for the additional equipment you will need.

Sincerely yours,

  
A. F. Rohlf

-ng

cc: JG Anderson  
EC Momnie  
EC Schrom  
FJ Turner

*To run Test*  
*\$2775 per Ed Schrom*  
*telephone 8/14/76*

*Fred Turner 8-736-3165 - says \$4000*



# GENERAL ELECTRIC

TRANSFORMER AND  
DISTRIBUTION  
EQUIPMENT  
BUSINESS DIVISION

GENERAL ELECTRIC COMPANY, 100 WOODLAWN AVE., PITTSFIELD, MASS. 01201  
Phone (413) 494-3577  
(EXT.)

August 12, 1976

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Sincerely yours,

  
A. F. Rohlf

-ng

cc: JG Anderson  
EC Momnie  
EC Schrom  
FJ Turner



Switching Surge Tent.

Fuel Turner ~~18<sup>th</sup>~~ 19<sup>th</sup> 25<sup>th</sup>

(3) 20 unit string 36.000 lb unit Brunelle

Rated critical impulse F.O. positive polarity  
Must equal 92% of rating 1210 kV, 1150 unit  
Oscilloscope required  
Wave shape 150/2500

Alt shipping instruction  
Use Petro Fuel Tank

He Valt Lal Bldg 9 -

100 woodland Ave

NY Petro Fuel 02201

Petro Fuel Tank

PO # 11/10/98 \$4000

Charge 29102-5-28-98



November 5, 1975

Dale Electronics  
1354 Twenty-eighth Avenue  
Columbus, Nebraska 68601

Gentlemen:

We are interested in purchasing noninductive card resistors for use with circuitry on impulse generators, and we understand you manufacture these items. We would, therefore, appreciate receiving a catalog, or other descriptive literature, together with pricing on these items.

Very truly yours,

Fred C. Vose  
Manager-High Voltage  
Laboratory

FCV/lan



November 5, 1975

Ohmite Manufacturing Company  
3604 Howood Street  
Skokie, Illinois 60076

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Manager-High Voltage  
Laboratory

FCV/lan

*Do not make card resistors  
per this letter*



November 5, 1975

Eastern Precision Resistor Division  
Cardwell Condense Corporation  
Lindenhurst, New York 11757

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FCV/lan



Gen = 37.5 K watt sec

Tuned in a Capacitor W

$$\frac{1}{2} C E^2 10^{-6}$$

energy in joules (watt seconds)

capacitance in microfarads

potential difference between electrodes  
in volts,

IRC Resistors - Internal resistors  
International Resistor Co  
Box 393 Boone N.C. 704-264-8861  
Balt Enterprise 9-3155

Eastern Precision Resistor Div.  
Cordell Anderson Corp.

Lindenhurst N.Y. 11757  
Tel 516-884-4300

Sold  
to Johnson in Baltimore



Ohrite Mfg Co.

Skokie, Ill.

3604 Howard St. 60076

312-675-2600

Dale Electronics Columbus, Neb

1354 - 28<sup>th</sup> Ave

68601

402-564-3131



Gen = 37.5 K watt sec

Energy stored in a Capacitor  $W$   
 $W = \frac{1}{2} C E^2 10^{-6}$

$W$  = energy in joules (watt seconds)

$C$  = Capacitance in microfarads

$E$  = potential difference between electrodes  
in ~~at~~ volts.

IRC Resistors - Internal resistors  
International Resistor Co

Box 393 Boone N.C.

704-264-8861

Balt Enterprise 9-3155



Bombs in parallel

$$V = LSV \times R_{\text{atto}} \times \sqrt{2} \times 2 \times 10$$

~~760,000~~

$$LSV = \frac{780,000}{143.2 \times 1.414 \times 20} = 192.6 \text{ Volts}$$



For 11 (71 KV)

$$W = \frac{1}{2} \times .33 \times \overline{71,000}^2 \times 10^{-6}$$

$$= 831 \text{ watt sec}$$

$$= .831 \text{ Kilowatt Sec}$$

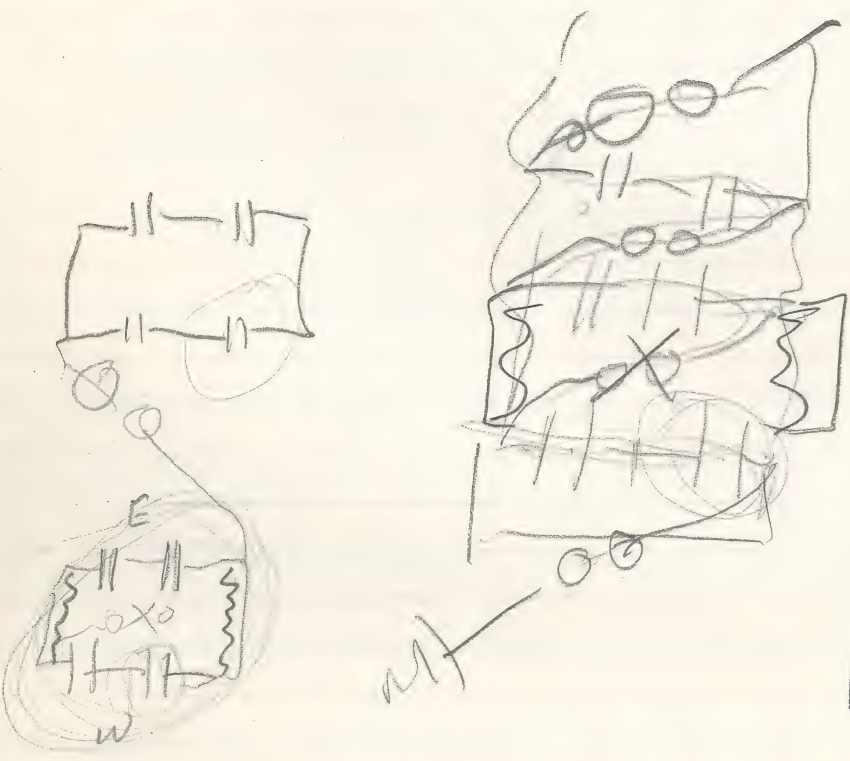
$$\text{Total } W = .831 \times 11 = 9.14 \text{ Kilowatt Sec}$$



$$40 \quad \left(\frac{1}{4}\right)$$

$$10 \times \frac{1}{2} \times \frac{1}{3} \times \frac{(78)^2}{(10)^6}$$

78x10



11. 11



Use (19) in parallel (38)

$$\text{Voltage} = 780/19 = 41 \text{ KV/can}$$

$$W = \frac{1}{2} \times .33 \times 41,000^2 \times 10^{-9} = .277 \text{ Kwatt sec}$$

$$\text{Total } W = .277 \times 38 = 10.526 \text{ Kwatt sec}$$

Use (18) in parallel

$$\text{Voltage} = 43.33 \text{ KV/can}$$

$$W = \frac{1}{2} \times .33 \times 43,333^2 \times 10^{-9} = .309 \text{ Kwatt sec}$$

$$\text{total } W = 36 \times .309 = 11.124$$

Use (16) in parallel (32)

$$\text{Voltage} = 780/16 = 48.75 \text{ KV/can}$$

$$W = \frac{1}{2} \times .33 \times 48750^2 \times 10^{-9} = .392 \text{ Kwatt sec}$$

$$\text{total } W = .392 \times 32 = 12.54 \text{ Kwatt sec}$$

Use 20 in parallel (40) cans

$$\text{Voltage} = 780/20 = 39 \text{ KV/can}$$

$$W = \frac{1}{2} \times .33 \times 39000^2 \times 10^{-9} = .250 \text{ Kwatt sec}$$

$$\text{Total } W = 40 \times .250 = 10.0 \text{ Kwatt sec}$$



Precision DC Supply

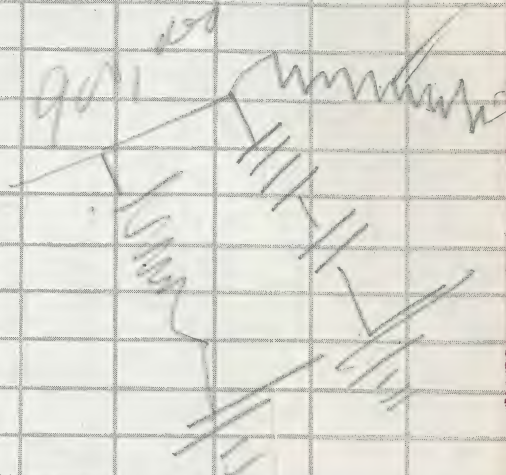
Model 301 E  
John Fluke Mfg Co.

Charging resistor 690K

11 975K

8-272-9202

Time _____	Date _____
WB _____	DB _____ Ser _____
RAD _____	VP _____ H _____



KV BANK	$\mu$ SEC / CM	R <sub>1</sub> POS	SCOPE TAP	C <sub>2</sub> MED	RATIO	POL	IMPULSES
CREST SCOPE VOLTS			CREST KILOVOLTS		CHOP TIME MICROSECONDS		REMARKS

Left Page

Right Page

Block 5 → 4

KV BANK	$\mu$ SEC / CM	R <sub>1</sub> POS	SCOPE TAP	C <sub>2</sub> MED	RATIO	POL	IMPULSES
LSV	50		Direct	3.77	3495	P <sub>01</sub>	F 0 F 0 40
Scope (visual)			CREST SCOPE VOLTS / cm	CREST KILOVOLTS	CHOP TIME MICROSECONDS		REMARKS
	430		385	2.8	KV / micro		0/0 F.O
Full wave					KV / micro		

2.8  $\mu$ V clipped more

$$= \frac{\text{Ratio} \times \text{scope volts}}{\text{microsec/cm} \times \text{cm from crest volt scope}} \rightarrow \text{cm}$$



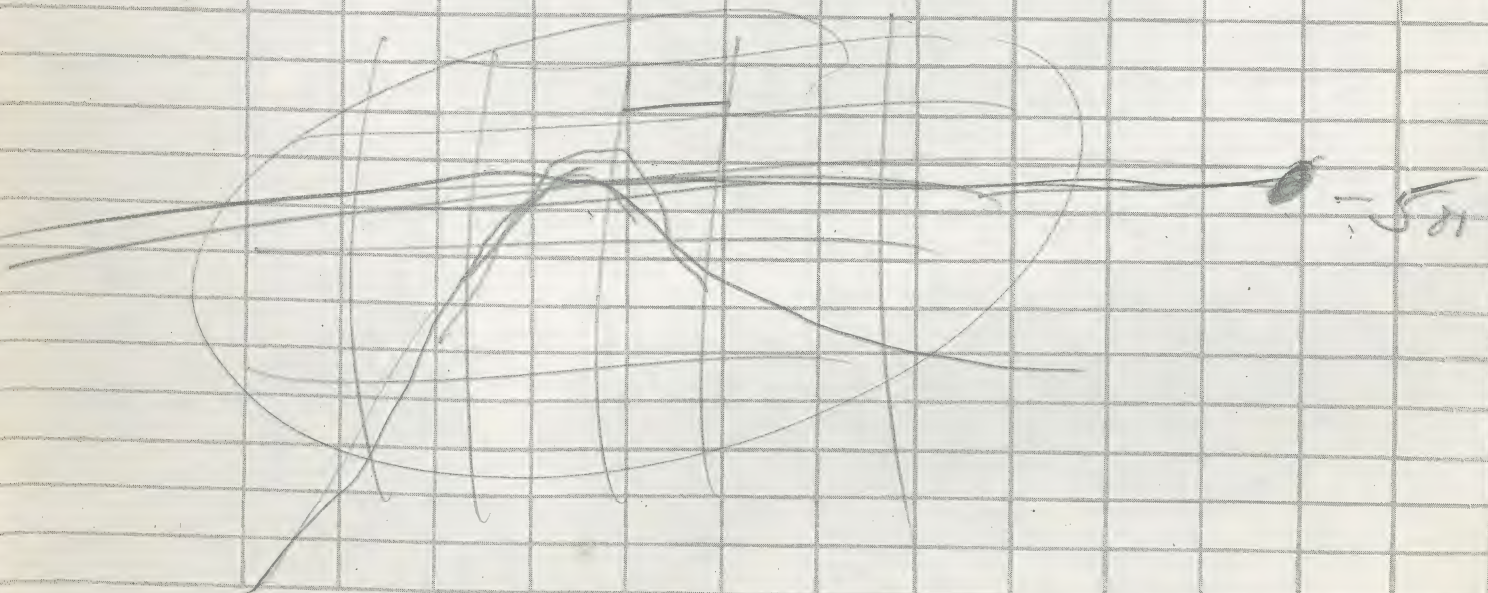
Take 20 shots record F.O. ~~and~~ or without, get  
 average without - and over crest F.O.  
 In taking readings crest rope volts /  
 $\frac{\text{time to chop}}{\text{it chop in cm}}$  then  $\frac{KV}{\text{microns}}$   
 $\times \frac{\text{microns}}{\text{cm}}$

Putting up make equal space for  
 Crest Rope Volts KV/microns

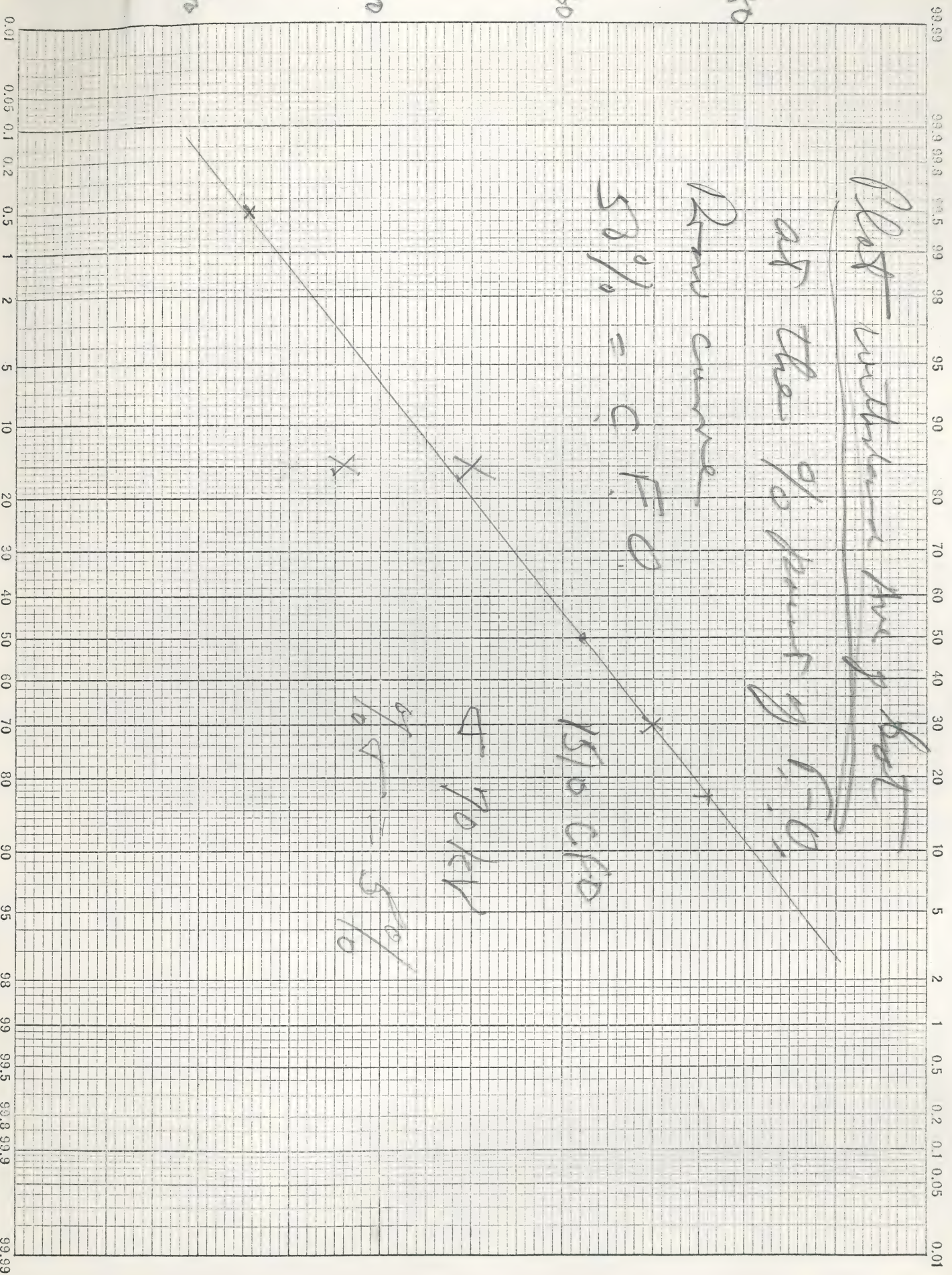
Plot Ave without of the 20 last shots and  
 curve

String Number	1st string total	- 1 - 20
Ground end	2nd	21 - 40
hot end	3rd	41 - 60

Ratometer Cost







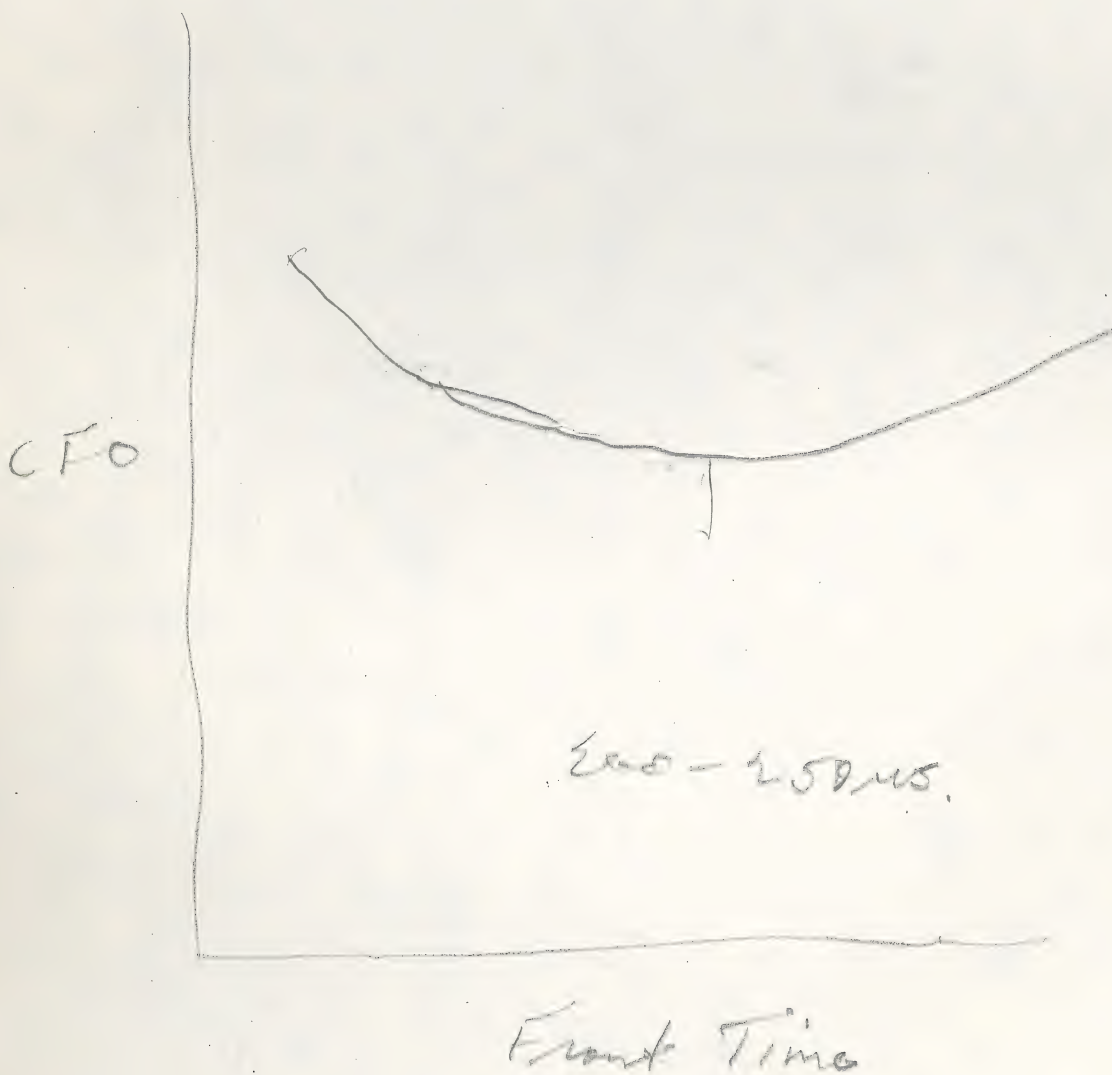
1300

1400

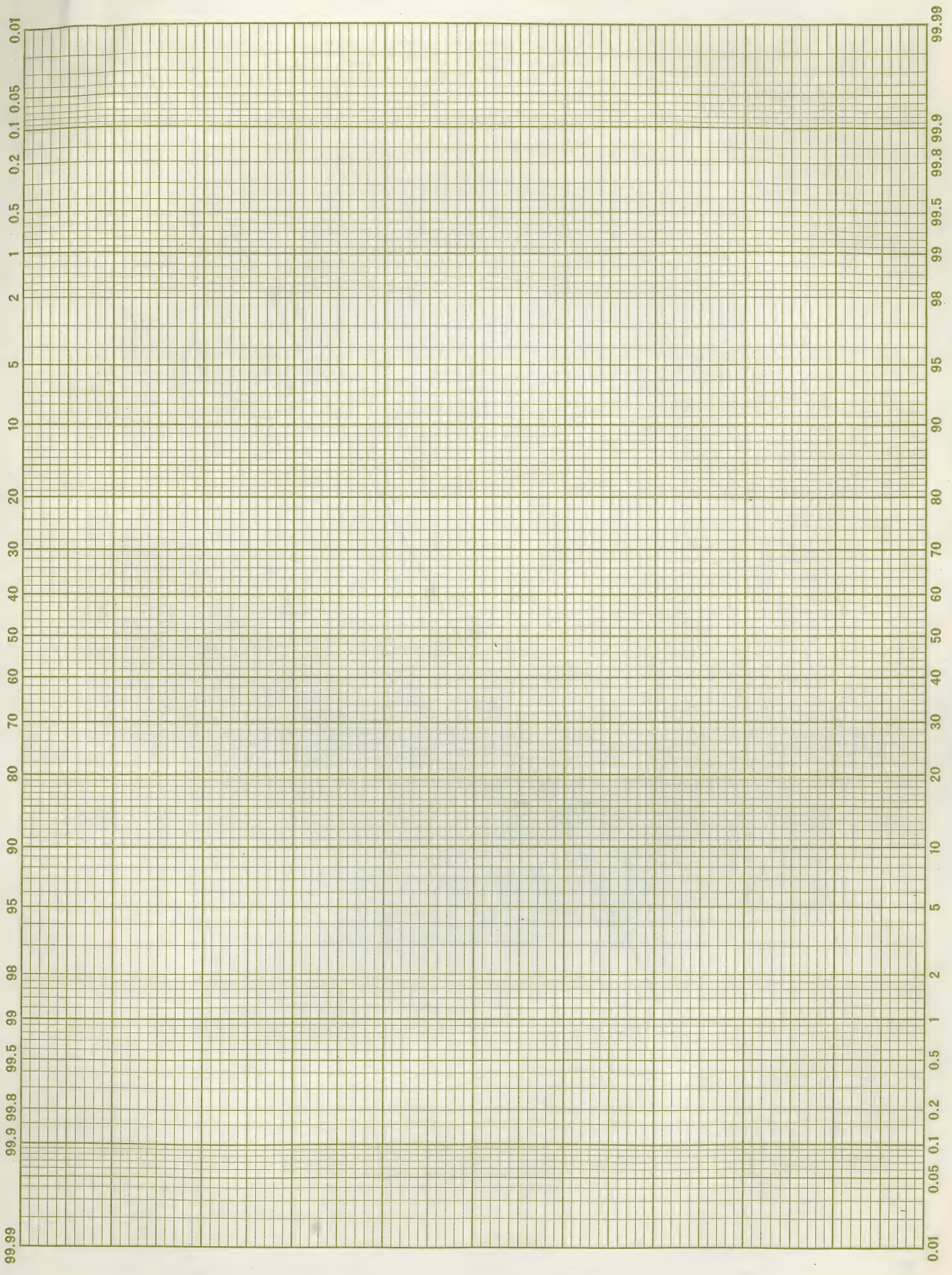
1500

1600

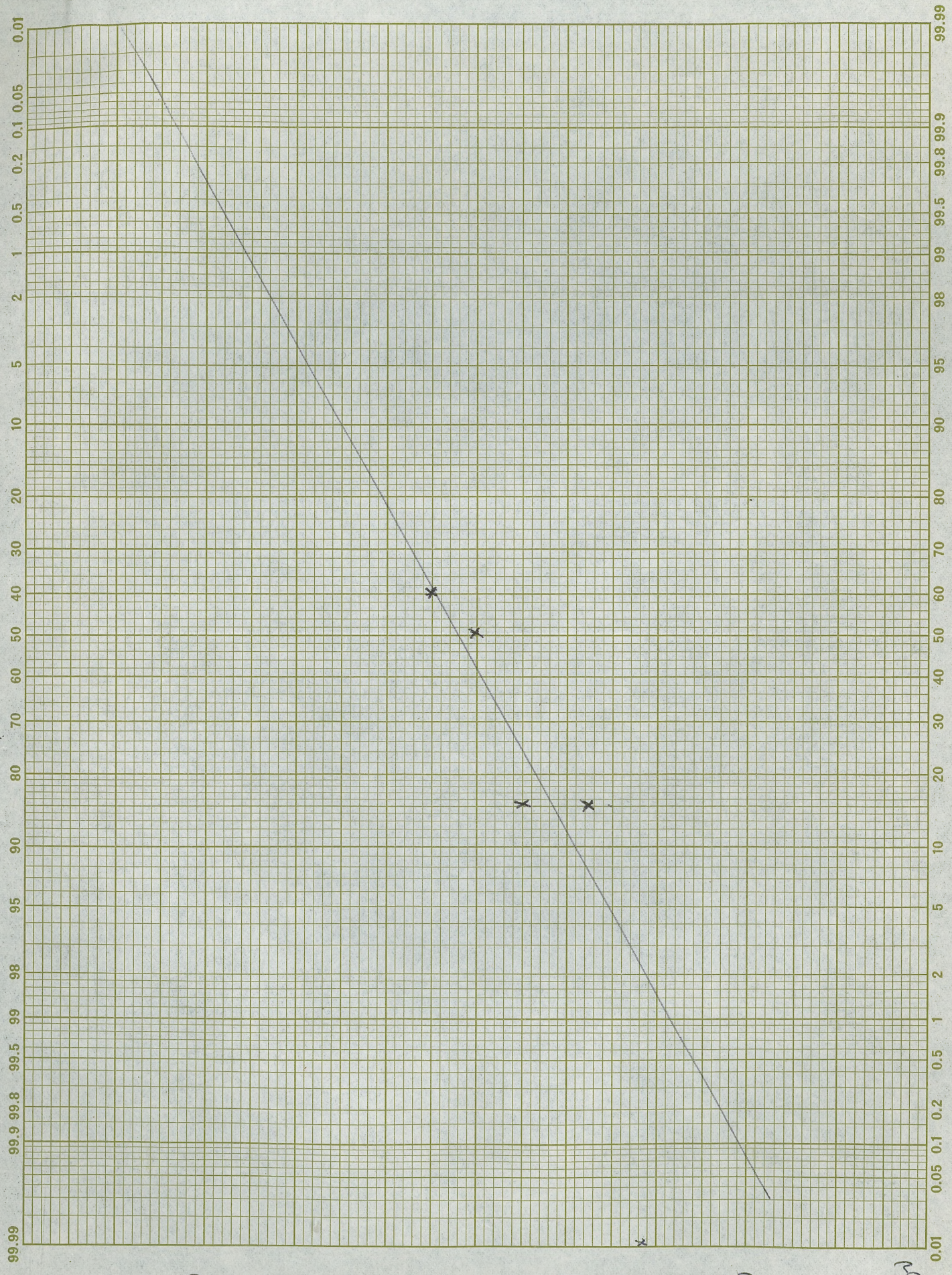












1800

2000

4000

1200

1000



# Development Authorization

Funds are requested to purchase the required materials and have ~~the~~ fabricated certain special components to give the High Voltage Laboratory the equipment to make Switching Surge Tests.

## Cost Analysis -

Item	Investment	Expense	Total
Series Resistor + clips	—	325	
Charging Resistor		725	
Bladder Resistor		400	
Capacitors and hardware		200	
Miscellaneous hardware		500	
Lab. for Making Capacitor boxes and Resistor Banks		800	
D.C. Power Supply	800	—	
Sub Totals	800	2950	
10% Contingency	80	295	
Totals	880	3245	4125

Vorey



$$\# \times \text{in} = \frac{\text{in} \#}{\text{in}} = \#$$

A hand-drawn sketch on aged, yellowish-brown paper. The sketch features a jagged, zig-zagging line that runs diagonally from the bottom left towards the top right. To the left of this line, the handwritten text 'R 200' is visible. Further along the line, there is a small circular mark containing the handwritten number '1000'. To the right of the main jagged line, there is another circular mark containing the handwritten letters 'H' and 'C'. The overall impression is that of a rough, preliminary drawing or map.


Pos. —  
neg. —

1321

47 32 17 2

(14:85

45 30 15 00



3.99  
72.4  
1.39

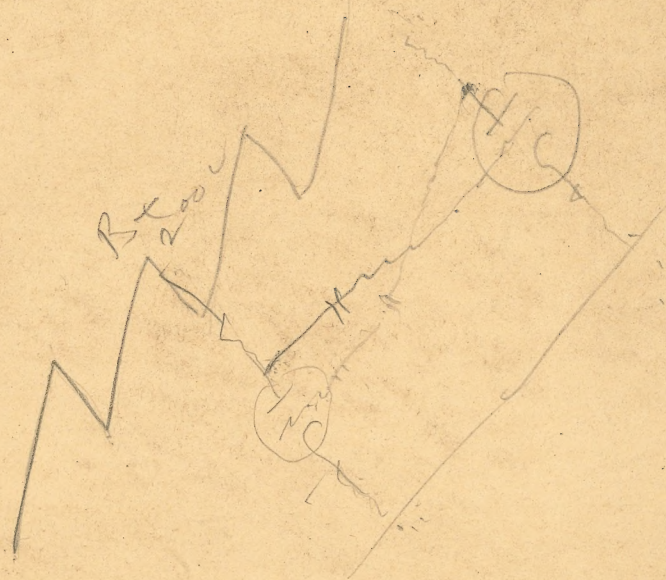
3.992  
72.4  
54.39

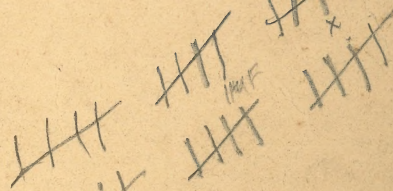
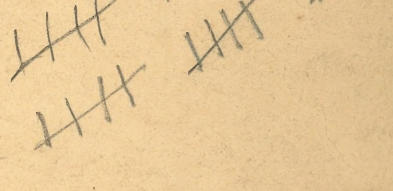
Impulse Generator



9" diam x 1" long

$$\# \times \text{in} = \frac{\text{in} \#}{\text{is}} = \#$$

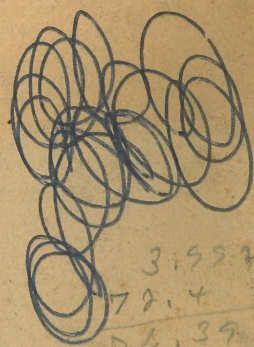


Pos. —   
 Neg. — 

35-28  
 35-21  
 49-14  
 28-14  
 28-21  
 7-14  
 35-7  
 63-49  
 35-14  
 49-35  
 49-21  
 21-28  
 35-42  
 49-28  
 121.73  
 27  
 84

7 2 7 12  
 5 4 1 2  
 47 32 17 2

14:85  
 45 30 15 00

  
 31924  
 72.4  
 72.32